



INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification ⁶ : C03B 19/00, 19/06, 37/018</p>	<p>A1</p>	<p>(11) International Publication Number: WO 99/15468</p> <p>(43) International Publication Date: 1 April 1999 (01.04.99)</p>
<p>(21) International Application Number: PCT/US98/18067</p> <p>(22) International Filing Date: 31 August 1998 (31.08.98)</p> <p>(30) Priority Data: 60/059,859 24 September 1997 (24.09.97) US</p> <p>(71) Applicant (for all designated States except US): CORNING INCORPORATED [US/US]; 1 Riverfront Plaza, Corning, NY 14831 (US).</p> <p>(72) Inventors; and (75) Inventors/Applicants (for US only): MAXON, James, E. [US/US]; 17 Wells Street, Canton, NY 13617 (US). PAVLIK, Robert, S., Jr. [US/US]; 110 West Third Street, Corning, NY 14830 (US). SEMPOLINSKI, Daniel, R. [US/US]; 5 Overbrook Road, Painted Post, NY 14870 (US). WASILEWSKI, Michael, H. [US/US]; 1617 Riff Road, R.D. #2, Corning, NY 14830 (US).</p> <p>(74) Agent: HERZFELD, Alexander, R.; Corning Incorporated, Patent Dept., SP FR 02-12, Corning, NY 14831 (US).</p>		<p>(81) Designated States: JP, KR, US, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).</p> <p>Published <i>With international search report.</i></p>
<p>(54) Title: FUSED SiO₂-TiO₂ GLASS METHOD</p> <div data-bbox="321 1157 1284 1629"> </div> <p>(57) Abstract</p> <p>A method of producing, by flame hydrolysis, a fused silica glass containing titania which comprises delivering a mixture of a silica precursor and a titania precursor in vapor form to a flame, passing the vapor mixture through the flame to form SiO₂-TiO₂ particles, and depositing the particles within a furnace (40) where they melt to form a solid glass body (44).</p>		

FOR THE PURPOSES OF INFORMATION ONLY

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AL	Albania	ES	Spain	LS	Lesotho	SI	Slovenia
AM	Armenia	FI	Finland	LT	Lithuania	SK	Slovakia
AT	Austria	FR	France	LU	Luxembourg	SN	Senegal
AU	Australia	GA	Gabon	LV	Latvia	SZ	Swaziland
AZ	Azerbaijan	GB	United Kingdom	MC	Monaco	TD	Chad
BA	Bosnia and Herzegovina	GE	Georgia	MD	Republic of Moldova	TG	Togo
BB	Barbados	GH	Ghana	MG	Madagascar	TJ	Tajikistan
BE	Belgium	GN	Guinea	MK	The former Yugoslav Republic of Macedonia	TM	Turkmenistan
BF	Burkina Faso	GR	Greece	ML	Mali	TR	Turkey
BG	Bulgaria	HU	Hungary	MN	Mongolia	TT	Trinidad and Tobago
BJ	Benin	IE	Ireland	MR	Mauritania	UA	Ukraine
BR	Brazil	IL	Israel	MW	Malawi	UG	Uganda
BY	Belarus	IS	Iceland	MX	Mexico	US	United States of America
CA	Canada	IT	Italy	NE	Niger	UZ	Uzbekistan
CF	Central African Republic	JP	Japan	NL	Netherlands	VN	Viet Nam
CG	Congo	KE	Kenya	NO	Norway	YU	Yugoslavia
CH	Switzerland	KG	Kyrgyzstan	NZ	New Zealand	ZW	Zimbabwe
CI	Côte d'Ivoire	KP	Democratic People's Republic of Korea	PL	Poland		
CM	Cameroon	KR	Republic of Korea	PT	Portugal		
CN	China	KZ	Kazakhstan	RO	Romania		
CU	Cuba	LC	Saint Lucia	RU	Russian Federation		
CZ	Czech Republic	LI	Liechtenstein	SD	Sudan		
DE	Germany	LK	Sri Lanka	SE	Sweden		
DK	Denmark	LR	Liberia	SG	Singapore		
EE	Estonia						

FUSED SiO_2 - TiO_2 GLASS METHOD

FIELD OF THE INVENTION

5 Method of producing fused silica glasses containing titania.

BACKGROUND OF THE INVENTION

10 Relatively pure metal oxides are produced by thermal decomposition of precursors and deposition of the resulting oxides. The precursor may take the form of a vapor, or may be carried by a vapor. It may be decomposed by either flame hydrolysis or pyrolysis.

15 One such process is production of fused silica by hydrolysis or pyrolysis of a silica precursor. Commercially, this is an application of flame hydrolysis involving forming and depositing particles of fused silica which melt to form large bodies (boules). Such boules may be used individually, may be finished and integrated together into large optical bodies, or may be cut into small pieces for finishing as lenses and the like. In this procedure, the precursor is hydrolyzed and the hydrolyzed vapor is passed into a flame to form particles of
20 a fused silica. The particles are continuously deposited, for example, in the cup of a refractory furnace where they melt to form a solid boule.

Essentially pure fused silica finds many diverse applications. However, it does have a small positive coefficient of thermal expansion (CTE) that can make it undesirable in some instances. United States Patent No. 2,326,059 (Nordberg) describes a fused silica doped with 5-11% by weight titania (TiO_2).

5 These TiO_2 -doped glasses have CTEs lower than pure fused silica with the potential for a CTE that approximates 0.

Originally, chlorides of silicon and titanium were employed as precursors. Recently, primarily for environmental reasons, chloride-free precursors have been proposed. Specifically, a siloxane,
10 octamethylcyclotetrasiloxane (OMCTS), and a titanium alkoxide, titanium isopropoxide, $\text{Ti}(\text{OPri})_4$, are commercially employed.

The precursors are separately converted to vapor form and carried to a mixing manifold by a carrier gas, such as nitrogen. The mixture passes, via fume lines, into a flame where the precursors are converted into SiO_2 - TiO_2
15 particles. These particles are collected in a refractory furnace where they melt to form a solid boule.

With the changeover to the new precursor materials, problems have been encountered. These problems are manifested largely by material build-ups in the vapor delivery system. The build-ups cause erratic operation, and
20 consequent furnace upsets. Ultimately, they require shut down of the vapor delivery system for cleaning.

It is a basic purpose of this invention to provide an improved method of producing a TiO_2 -doped fused silica.

Another purpose is to minimize material build-ups that occur in the
25 vapor delivery system during operation.

A further purpose is to improve the quality of the TiO_2 -doped fused silica produced.

A still further purpose is to lengthen the time of a production run before it is necessary to shut the operation down for cleaning purposes.

SUMMARY OF THE INVENTION

5 Broadly, the invention resides in a method of producing, by flame hydrolysis, a fused silica glass containing titania which comprises delivering a mixture of a silica precursor and a titania precursor in vapor form to a flame, passing the mixture through the flame to form $\text{SiO}_2\text{-TiO}_2$ particles, and delivering an essentially pure, titanium precursor to the flame.

BRIEF DESCRIPTION OF THE DRAWINGS

10

The single FIGURE in the accompanying drawing is a schematic representation of a system for practice of the invention.

PRIOR ART

15

Literature deemed of possible relevance is listed in an accompanying document.

DESCRIPTION OF THE INVENTION

20

25 The conventional, boule process used in making fused silica products is a continuous process. In this process, a carrier gas, such as nitrogen, is bubbled through a silica precursor, such as SiCl_4 , or OMCTS. The carrier gas entrains the precursor in vapor form and transports it to the site of the flame hydrolysis.

25

30 Production of a $\text{SiO}_2\text{-TiO}_2$ glass follows the same basic procedure, but a titania precursor is introduced. Essentially, this involves duplicating the delivery system for the silica precursor to provide entrained vapors of the titania precursor. The two separate vapor trains feed into a manifold where they are mixed. The mixture is then carried through fume lines to burners where the flame hydrolysis takes place.

The flame converts the mixture of precursors into particles of TiO_2 -doped silica, commonly referred to as "soot." The particles form within a refractory furnace having a member in its base known as a cup. The particles are deposited in the cup, and melt to form a solid body referred to as a boule.

5 The single FIGURE in the accompanying drawing is a schematic representation of a system for use in practicing the present invention. The system is generally designated by the numeral 10.

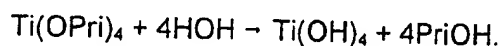
10 System 10 includes a source 12 of the silica precursor 14. A carrier gas 16, such as nitrogen, is introduced at or near the base of source 12. A by-pass stream of carrier gas is introduced at 18 to prevent saturation of the vaporous stream. The vaporous stream passes through a distribution system 20 to a manifold 22.

15 System 10 further includes a source 24 of the titania precursor 26. Source 24, like source 12, has an inlet 28 for a carrier gas that passes through precursor material 26 and entrains vapors thereof. Again, a bypass stream is introduced at 30, and the vaporous stream passes through a distribution system 32 to manifold 22.

20 The two vapor streams mix in manifold 22. The mixture passes through fume lines 34 to burners 36 mounted in the upper portion 38 of furnace 40. The mixed vapor stream is further joined with a fuel/oxygen mixture at burners 36. There it combusts and is oxidized to form silica-titania particles at a temperature in excess of 1600°C . The particles thus formed are directed at, and collect in, cup 42 of refractory furnace 40. There, they melt to form a solid boule shown as 44.

25 The present invention arose when efforts were made to convert the system and process from chloride precursors to the more environmentally friendly, metallo-organic precursor materials (OMCTS and titanium isopropoxide). The alkoxides of the transition metals were known to be sensitive to light, heat and moisture. It was also known that the metal
30 alkoxides readily hydrolyze with moisture to form the hydroxide and oxide of the metal.

Accordingly, when white deposits built up in the vapor delivery system, it was suspected that moisture was the culprit. Thus, it was postulated that these reactions were occurring:



5



This led to a search for a source of moisture.

Surprisingly, the silica precursor, OMCTS, was found to be the source of moisture. Accordingly, it has been found necessary to employ "dry" OMCTS in the present process. In particular, it has been necessary to maintain the water content in the OMCTS at less than 2 ppm. to inhibit the white, titania build-up in the system.

10

It has also been found necessary to carefully control temperature in the vapor distribution system. This is particularly true in the fume lines 34 between manifold 22 and burners 36. If these lines are too cold, vapors can condense in the line and disrupt flow. This situation is averted by exposing the fume lines to heat from the burners and the furnace crown.

15

If the temperature in the fume lines becomes too high, titanium isopropoxide tends to thermally decompose, thus forming oxide deposits in the line. The oxide deposits disrupt vapor flow and cause turbulence in the furnace atmosphere. As shown later, this contributes to other problems in the furnace.

20

To avoid this overheating problem, fume lines 34 are preferably insulated. For example, the lines may be clad with a highly conductive and reflective material such as aluminum foil.

25

It has been observed that crown 46 of furnace 40 runs hottest in its central area. As a result, a glassy condensate tends to develop in this area. In time, this condensate can build-up and form a stalactite-like shape. Ultimately, drippage onto the fused silica boule from this glassy stalactite can occur. This creates effects in the boule that must be removed by grinding. To avoid this expensive process, the boule lay-down cycle is shortened, thus adding to the cost of the operation.

30

At least two conditions have been found to aggravate development of the glassy condensate in the center of the crown. One condition is impurities in the refractory brick, especially alkali and alkaline earth metal impurities. As such impurities migrate from the brick, or the silica penetrates the brick, a less viscous, more fluid glass develops. This in turn more readily flows and drips onto the boule. This contributing factor can be minimized by employing pure materials in brick preparation; also by treatment of the furnace bricks to extract impurities prior to use of the furnace.

The other condition manifests itself within the furnace, but it is caused by conditions in the vapor delivery system. The condition is turbulence in the furnace due to eddy currents developed in the flame. A key to controlling turbulence has been found to be maintenance of smooth, vapor flow rates.

This requires more than mere inlet valve regulation and temperature control of the precursor materials. It has previously been explained that moisture must be essentially excluded to avoid dissociation of titanium alkoxide, and consequent buildup on the distribution system walls. It has been found that such buildup also creates erratic flow rates. These, in turn, cause turbulence in the furnace atmosphere.

Titanium alkoxides, particularly $\text{Ti}(\text{OPri})_4$, are water white in a pure state, but degrade readily. This condition is exhibited by a discoloration in the material that proceeds from a pale yellow through amber to dark brown. The discoloration is due to such contaminants as higher order polymers, oxidation products, and trace elements. As the alkoxide degrades, its properties change. In particular, its vapor pressure changes. This alters the flow-rate and thereby causes turbulence as well as composition variation. The turbulence, as noted, aggravates the buildup of glass condensate in the center of the furnace crown.

An added benefit of using a pure titanium alkoxide is that it permits using higher temperatures in the precursor materials. The vapor pressure of the alkoxide increases with temperature, thus requiring a lower, carrier vapor

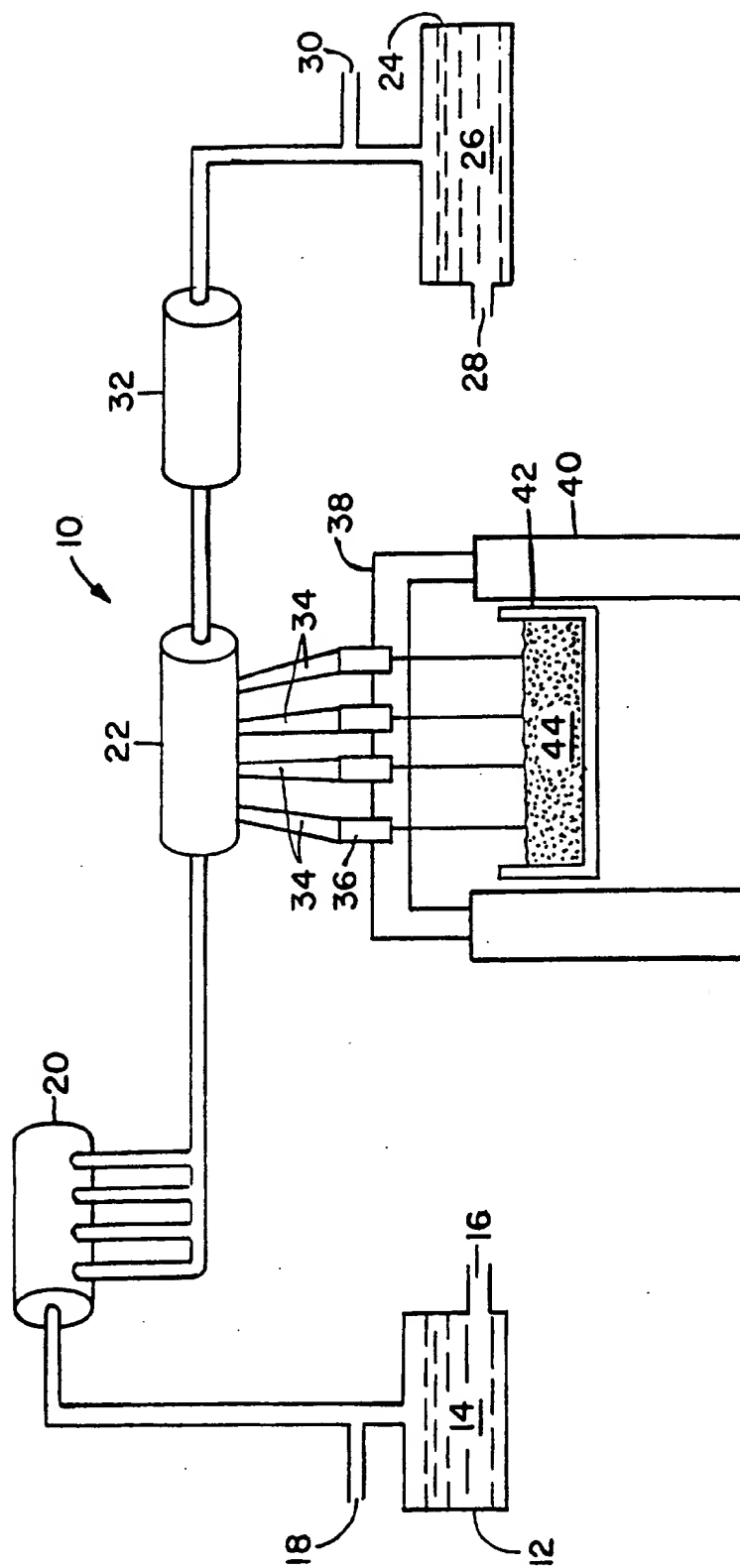
flow rate. This lower flow rate contributes to a smoother operation and less turbulence.

In summary then, optimum production of a fused, $\text{SiO}_2\text{-TiO}_2$ glass product by flame hydrolysis is obtained by using a relatively pure, titania precursor and a relatively dry, silica precursor. Also, decomposition of the titania precursor should be avoided by controlling the temperature in the fume lines. Finally, the brick in the furnace, particularly in the crown portion, should be purified to minimize the occurrence of glass condensate at the crown hot spot.

WE CLAIM:

1. In a method of producing, by flame hydrolysis, a fused silica glass containing titania which comprises delivering a mixture of a silica precursor
5 and a titania precursor in vapor form to a flame and, passing the mixture through the flame to form $\text{SiO}_2\text{-TiO}_2$ particles, the improvement which comprises delivering an essentially pure, titanium precursor to the flame.
2. A method in accordance with claim 1 which comprises delivering
10 precursors composed essentially of a siloxane and a titanium alkoxide.
3. A method in accordance with claim 2 which comprises delivering octametylcyclotetrasiloxane and titanium isopropoxide to the flame.
- 15 4. A method in accordance with claim 2 which comprises delivering a siloxane that contains less than 2 ppm. water.
5. A method in accordance with claim 2 which comprises delivering a
20 titanium alkoxide that is essentially colorless.
6. A method in accordance with claim 1 which comprises depositing the $\text{SiO}_2\text{-TiO}_2$ particles in a refractory brick furnace while minimizing turbulence in the furnace atmosphere during deposition.
- 25 7. A method in accordance with claim 6 which comprises maintaining steady, vapor flow rates during delivery of the precursors to the flame for hydrolysis.
8. A method in accordance with claim 7 which comprises avoiding
30 decomposition or condensation of the titania precursor to form deposits in the vapor delivery lines.

- 5 9. A method in accordance with claim 8 which comprises maintaining the titanium precursor vapor at a temperature above its condensation point, but below its decomposition temperature, during its delivery to the flame for hydrolysis.
- 10 10. A method in accordance with claim 9 which comprises delivering the mixture of precursors through insulated fume lines to avoid overheating and decomposition of the titanium precursor.
11. A method in accordance with claim 10 which comprises delivering the precursors through fume lines insulated with a heat conducting and reflecting cladding.
- 15 12. A method in accordance with claim 11 which comprises delivering the precursors through fume lines clad with aluminum foil.
- 20 13. A method in accordance with claim 1 which comprises depositing the $\text{SiO}_2\text{-TiO}_2$ particles in a refractory brick furnace in which at least the furnace crown is composed of purified brick to minimize the effect of silica condensate forming on the crown.
- 25 14. A method of producing, by flame hydrolysis, a fused silica glass containing titania which comprises separately delivering vapor streams from sources of a silica precursor that contains less than 2 ppm. water, and a titania precursor that is essentially colorless, mixing the vapor streams, delivering the mixture to burners through fume lines while maintaining steady, vapor flow rate by controlling temperature of the fume lines, passing the mixture through the flame to produce $\text{SiO}_2\text{-TiO}_2$ particles, depositing the particles in a refractory furnace having at least its crown portion composed of purified brick, and
30 melting the particles as they are collected to form a solid body of fused silica.



INTERNATIONAL SEARCH REPORT

International application No.

PCT/US98/18067

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) :C03B 19/00, 19/06, 37/018

US CL :65/17.4, 414

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 65/17.3, 17.4, 32.4, 60.1, 60.5, 60.8, 414, 416, Dig. 8; 501/38, 53

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X --- A	US 5,154,744 A (BLACKWELL ET AL.) 13 October 1992, see entire document.	1-3 --- 4-14
X --- A	US 5,152,819 A (BLACKWELL ET AL.) 06 October 1992, see entire document.	1-3 --- 4-14
A	US 5,043,002 A (DOBBINS ET AL.) 27 August 1991, see entire document.	1-14
A	US 5,395,413 A (SEMPOLINSKI ET AL.) 07 March 1995, see entire document.	13

☐ Further documents are listed in the continuation of Box C.
 ☐ See patent family annex.

* Special categories of cited documents:	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
A document defining the general state of the art which is not considered to be of particular relevance	*X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
E earlier document published on or after the international filing date	*Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	*Z* document member of the same patent family
O document referring to an oral disclosure, use, exhibition or other means	
P document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

04 NOVEMBER 1998

Date of mailing of the international search report

31 DEC 1998

 Name and mailing address of the ISA/US
 Commissioner of Patents and Trademarks
 Box PCT
 Washington, D.C. 20231

Facsimile No. (703) 305-3230

Authorized officer

STEVEN P. GRIFFIN

Telephone No. (703) 308-0661

